



Devices thru Material Innovation

NEC/TOKIN

Vol.06

Transformer

Transfo



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INTRODUCTION

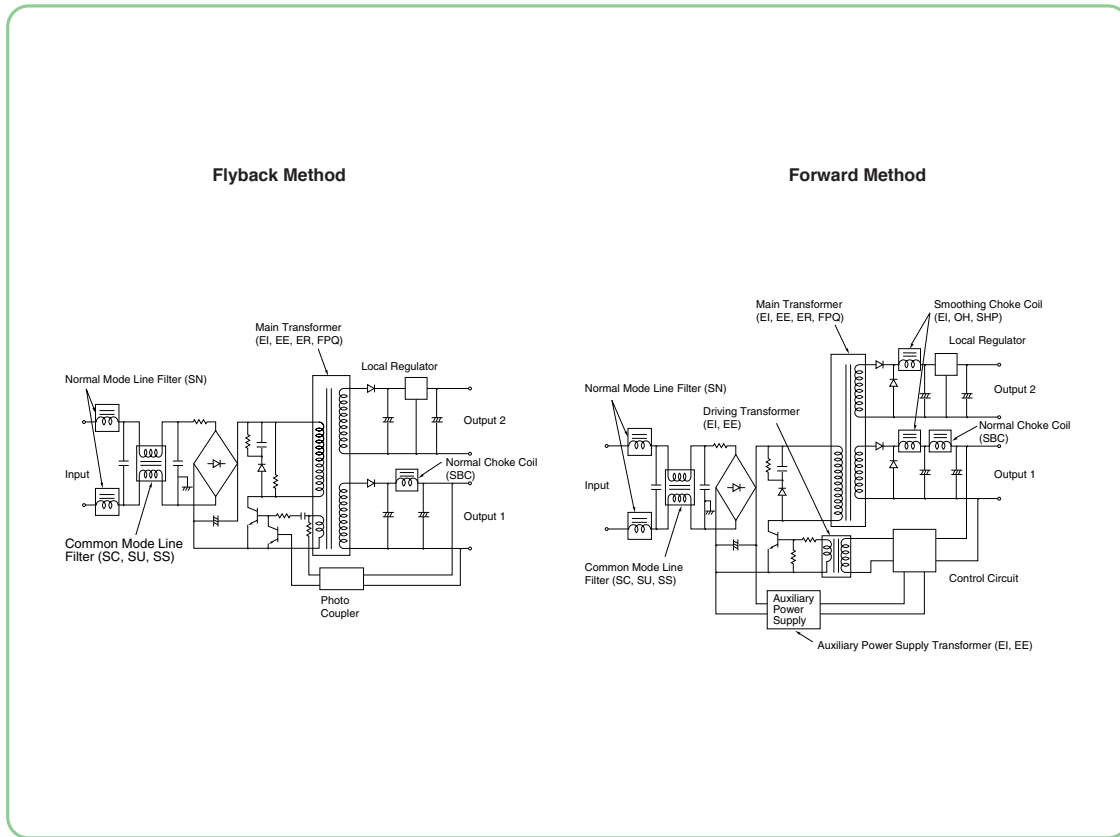


As semiconductor devices become ever more advanced, the demand for thinner, more compact devices with higher efficiency and functionality are increasing. Owing to technologies such as high-density mounting for the switching power supplies, requirements for transformers and chokes are becoming increasingly rigorous. Under the motto "Reliability based on high quality material," NEC TOKIN uses selected excellent materials to provide diverse transformers and choke coils that can meet the requirements for a wide range of applications, such as small toroidal structure types with little heat effect and minimal emission noise to peripheral parts.



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Example of Use



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Materials for Design

Design Method

At present, there are two major types of circuits for the typical switching power supply units: the forward converter method and the flyback method. (See Figure 1.)

The following section introduces the design method of the high frequency transformers for each of the two types mentioned above.

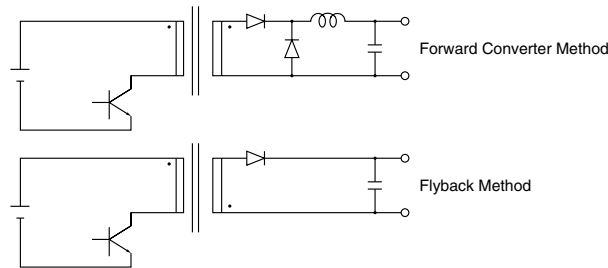


Figure 1 Circuit Method of Switching Power Supply

(1)Forward Converter Method 1)Transformers

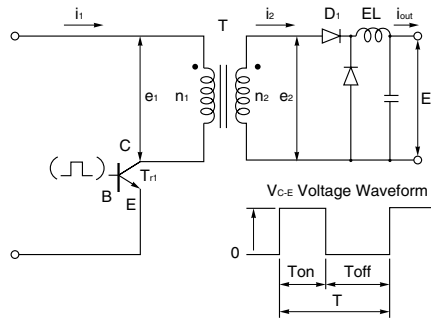


Figure 2 Circuit Diagram of Forward Converter

Figure 2 is the basic circuit diagram of the forward converter method.

When the bias (pulse) of forward direction is applied to the base of the switching transistor (Tr_1), Tr_1 is ON, e_1 (V) is impressed to the primary windings n_1 of the transformer "T", and at the same time the voltage as found by the following formula is generated to the secondary windings n_2 :

$$e_2 = \frac{n_2}{n_1} \times e_1(V) \dots\dots\dots \textcircled{1}$$

- e_1 : Input voltage of transformer
- e_2 : Output voltage of transformer
- n_1 : Number of primary windings
- n_2 : Number of secondary windings



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Therefore, the output voltage is found by the ratio of n_1 and n_2 . Also, from the law of equal ampere turns, the following formula is obtained:

$$i_2 = \frac{n_1}{n_2} \times i_1 \text{ (A)} \dots\dots\dots ②$$

The primary winding is determined by the following formula:

$$n_1 = \frac{e_1 \times T_{on}}{\Delta B \times A_e} \times 10^4 \dots\dots\dots ③$$

- Ton: Transistor (Tr1) "on" time (sec)
- ΔB : Usage magnetic flux density (T)
- Ae : Core effective cross-section (cm²)

At this point it is important to be aware of the value of ΔB. It must be set especially carefully, because when the magnetic flux is saturated, the inductance drops abruptly, in addition to the core loss and temperature rise. The magnetic flux density available for use is within the range from effective saturation magnetic flux density (Brms) to the effective saturation residual coercive force (Brms). However, it is necessary to set this value ΔB as shown below, considering the inevitable factors such as calorific value of the core:

1. Set the upper limit of allowable temperature of core heat.
2. The energy (Wattage) equivalent to the core loss at that time (set in the previous step 1).
3. The next time that same loss occurs and at what value (T).

According to the above stated procedure, the appropriate ΔB can be set.

The characteristics of the NEC TOKIN BH2 compound are shown in Figures 3 and 4.

Then, determine the output voltage "e2" of the transformer from the desired output voltage "Eo".

$$e_2: \frac{E_o}{\text{duty}} + (e_d + e_l) \dots\dots\dots ④$$

- duty: T_{on} / T $T = T_{on} + T_{off}$
- ed : Output rectification diode loss voltage (V)
- el : Line loss voltage (V)

The number of secondary windings is determined by formula ①

$$n_2 = \frac{e_2 \cdot n_1}{e_1}$$

When the number of secondary windings is determined, again modify the value of "n1", the number of primary windings:

$$n_1 = \frac{e_1 \cdot n_2}{e_2} \dots\dots\dots ⑤$$

At that time, it may be very convenient if the values ΔB, core loss and temperature rise of core are found.

Then determine the current i_2 applied to the secondary windings:

$$i_2 = \frac{i_{out}}{\text{duty}} \dots\dots\dots ⑥$$

The primary current is determined by formula w.



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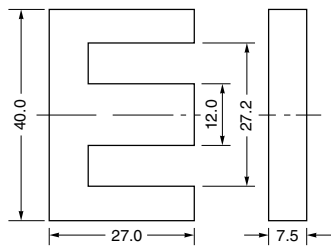
$$i_1 = \frac{n_2 \cdot i_2}{n_1}$$

The material of windings is determined by the following formula:

$$d\phi = \sqrt{\frac{4 \cdot i}{\delta \cdot \pi}} \dots\dots\dots ⑦$$

- dφ : Diameter of winding (mmφ)
- δ : Density of current (A/mm²)
- i : Average current (A)

When the current is large, the winding becomes very thick. Considering the bobbin structure and the efficiency of work, it is more convenient to use numerous windings with the diameter not exceeding 1.0. The higher the frequency used, the greater the loss by the skin effect of the windings. Therefore, applying many of the thinner windings instead of using the single thick winding is recommended.



Core Constant	Σ ℓ / A	cm ⁻¹	5.19
Effective Cross-section Area	Ae	cm ²	1.48
Effective Magnetic Circuit Length	ℓ e	cm	7.68
Effective Volume	Ve	cm ³	11.4
Cross-section Area of Middle Leg	Acp	cm ²	1.36
Core Frame Area	Acw	cm ²	1.63
Weight		g/set	61.0
AL		nH	4750

Figure 3 FEI40 (BH2) Core Constant

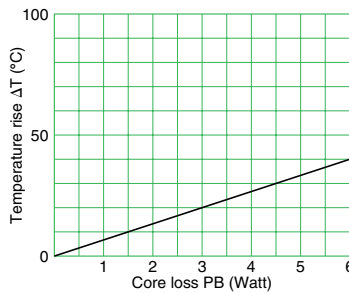


Figure 4 FEI40 core loss - temperature characteristics

2)Choke coils

Because the switching regulator's secondary side choking circuit is superimposed with direct current, a choke coil with good direct current superimposition characteristics must be selected to prevent saturation of the core. Therefore, for designing choke coils the data on the relationship between the gap and AL value is required.

For example, if the gap of the FEI40 (BH2) is 0.2 mm, then from Figure 5 showing the relationship of the FEI40's air gap AL, the AL value is 800nH. In this case, from the direct current superimposition characteristics it is understood that the range in



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which the direct current magnetic field's magnetic permeability does not decrease is 40AT. For making a choke coil, the following formula must apply between the actual number of windings N_1 and the maximum direct current superimposition current I_0 :

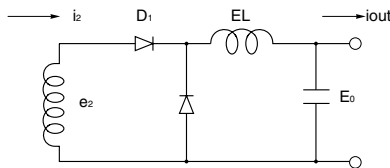
$$NI > N_1 I_0 \dots\dots\dots \textcircled{8}$$

Thus, in this case the number of windings and current capacity are selected according to $40AT > N_1 I_0$. On the other hand inductance is represented by the following formula:

$$L = AL \cdot N^2 \cdot 10^{-9} \text{ [H]} \dots\dots\dots \textcircled{9}$$

$$N = \sqrt{\frac{L \cdot 10^9}{AL}} \text{ (Turn)} \dots\dots\dots \textcircled{10}$$

When choosing the choke with the switching regulator, considering from the previous example :



$$eL = e_2 - e_d - E_o$$

$$= L \frac{di}{dt}$$

$$\therefore L = \frac{eL dt}{di} = \frac{eL \cdot T_{on}}{I_{out}}$$

Here, on account of the ripple and dummy load of I_{out} , general guidelines for the inductance of the output choke are derived using the following formula:

$$L = \frac{5E_o \cdot T_{on}}{I_{out} \text{ (max)}} \text{ [H]}$$

When a 0.1 mm gap is placed in the core's middle leg, the total gap is 0.1 mm, but when a 0.1 mm gap material is inserted overall, the total gap amount becomes 0.2 mm.

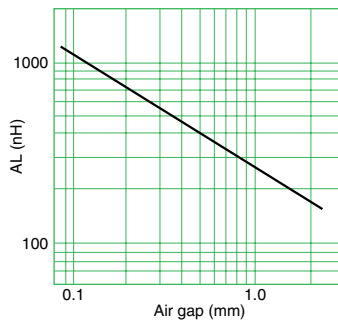


Figure 5 Air gap-AL characteristics (FEI40, BH2)



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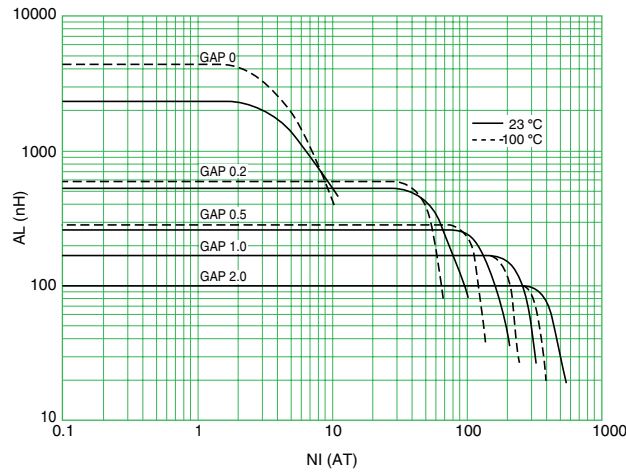


Figure 6 Direct current superimposition characteristics (FEI40, BH2)

(2) Flyback Method

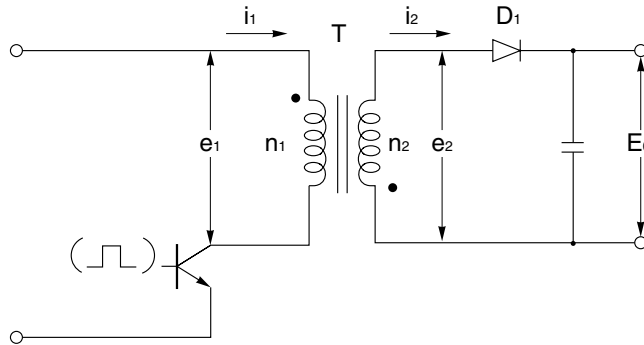


Figure 7 Circuit diagram of flyback method

The above Figure 7 is the circuit diagram of the flyback method. It is almost the same as the previous Figure 2 except for the polarity of the transformer. As the diode D_1 is located in the backward direction on the secondary output circuit, nothing is output when the switching transistor Tr_1 is turned ON. At that time, the following amount of energy is charged in the transformer T .

$$E = 1/2 Li^2 \dots\dots\dots(11)$$

L: Primary inductance (H)

The above energy is emitted to the load R by way of the secondary diode D_1 when Tr_1 is turned OFF. Determine the primary average current.

$$i_1 = \frac{E_o \cdot I_o}{e_1 \cdot \eta} \dots\dots\dots(12)$$

E_o : Output voltage
 I_o : Output current
 η : Energy conversion rate



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Determine the primary peak current $i_1 \text{ max.}$ by the following formula:

$$i_1 \text{ max.} = \frac{2 \cdot i_1 \cdot T}{T_{on}} \dots\dots\dots(13)$$

T: Driving cycle of switching (sec)

The inductance "Lp" necessary for the primary windings "n1" is determined by the following formula:

$$L_p \text{ min.} = \frac{e_1 \text{ min.} \cdot T_{on} \text{ max.}}{i_1 \text{ max.}} \text{ [H]} \dots\dots\dots(14)$$

The number of primary windings "n1" is determined by the following formula:

$$n_1 = \frac{L_p \text{ min.} \cdot i_1 \text{ max.}}{A_e \cdot \Delta B} \cdot 10^4 \dots\dots\dots(15)$$

In this case, a certain Gap is provided by the core. Therefore, its hysteresis curve becomes linear, unlike the nonlinear one for Gap = 0, and the value ΔB can be kept somewhat larger than the case using the forward method.

The number of secondary windings "n2" is determined by the following formula:

$$n_2 = \frac{n_1 \cdot (E_o + e_d + e_l)}{e_1} \cdot \frac{T_{off}}{T_{on}} \dots\dots\dots(16)$$

e_d : Secondary side diode loss voltage (V)
 e_l : Line loss voltage (V)

In the RCC method, the feedback winding is determined by the voltage "Ez" of the driving voltage, as shown in the following formula:

$$n_d = \frac{E_z + E_{BE}}{e_2 \cdot n_2} \dots\dots\dots(17)$$

The designing procedure has been completed by the above steps. However, a slight correction is actually required because of the differences from the various conditions initially set together with the linkage inductance of the transformer, floating capacity and transformer connecting conditions.

In recent years, the driving frequency has risen.

$$N_p = \frac{e_1 T_{on}}{\Delta B \cdot A_e} \times 10^4 \dots\dots\dots(18)$$

The higher it becomes, the fewer windings are required to enable the transformer to be downsized, as shown in the above formula. However, loss could increase by the skin effect of the winding material, as it does for the high frequency. In addition, it might be difficult to cope with the safety standards of each country. Therefore, it is necessary to select the method that is the most appropriate for the various conditions required for each transformer when selecting the winding materials, winding order, winding method and insulation structure.

To select the core, attention must be paid to the following items.

1. The magnetic flux density is to be high.
2. The core loss is to be low.



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3. The magnetic permeability is not to decrease within the driving frequency range.
- 4 The Curie temperature is to be high.
- 5 The saturation magnetic flux density is not to be abruptly changed by the temperature.

Table 1 shows the material characteristics of TOKIN's ferrite cores.

Table 1 Ferrite Core Material Characteristics

Material Characteristics		Unit	BH1	BH2	
Applied Frequency Range		MHz	<0.3	<0.3	
Initial Permeability	μ_i		2300±20%	2300±20%	
Effective Saturation Magnetic Flux Density (Approx.1200 A/m)	B _{ms}	23°C	520	510	
		100°C	410	400	
Effective Retentivity	B _{rms}	23°C	100	100	
		100°C	55	55	
Effective Coercivity	H _{cms}	23°C	13	14.3	
		100°C	5		
Curie Temperature	T _c	°C	220	220	
Core Loss	100kHz 200mT	P _{cv}	23°C	550	600
			60°C	350	450
			100°C	250	410
	500kHz 200mT	P _{cv}	23°C		
			60°C		
			100°C		
1MHz 50mT	P _{cv}	60°C			
		100°C			
Density	d	kg/m ³	4.8 × 10 ³	4.8 × 10 ³	



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Transformers/Choke Coils Series [RoHS Compliant]

Series	Shape of Core	Output Wattage				
		Forward Method		Flyback Method		
		50kHz(W)	100kHz(W)	50kHz(W)	100kHz(W)	
FEI·FEE	FEI12.5	3 to 8	4 to 10	2 to 5	3 to 6	
	FEI16	10 to 15	13 to 19	3 to 8	4 to 10	
	FEE16					
	FEI19	12 to 18	15 to 23	5 to 10	6 to 13	
	FEE19					
	FEI22	15 to 20	19 to 26	8 to 15	10 to 19	
	FEE22					
	FEI22S	15 to 20	19 to 26	8 to 15	10 to 19	
	FEI25	20 to 30	26 to 39	10 to 20	13 to 26	
	FEI28	30 to 50	40 to 65	20 to 30	25 to 40	
	FEI30	50 to 70	65 to 90	30 to 40	40 to 50	
	FEE30					
	FEI33	80 to 130	100 to 165	35 to 50	45 to 65	
	FEE33					
	FEI35S	80 to 130	100 to 165	35 to 50	45 to 65	
FEI40	100 to 150	130 to 195	45 to 75	60 to 95		
FEE40	90 to 140	115 to 180	40 to 70	50 to 90		
FEER	FEER25.5	20 to 30	26 to 39	10 to 20	13 to 26	
	FEER28	35 to 45	45 to 55	20 to 30	26 to 39	
	FEER28L	40 to 60	50 to 80	30 to 40	40 to 50	
	FEIR30	30 to 50	40 to 65	25 to 35	33 to 45	
	FEER35	70 to 100	90 to 130	40 to 50	50 to 65	
	FEER35L	100 to 150	130 to 195	50 to 65	65 to 80	
	FEER39L	130 to 200	170 to 260	70 to 90	90 to 115	
	FEER40	140 to 220	180 to 285	75 to 95	100 to 120	
	FPQ	FPQ2016-T-22	20 to 30	26 to 39	10 to 20	13 to 26
		FPQ2020-T-22	25 to 35	32 to 45	15 to 25	19 to 32
FPQ2620-T-22		45 to 60	60 to 75	25 to 35	32 to 45	
FPQ2625-T-22		50 to 70	65 to 90	30 to 40	40 to 50	
FPQ3220-T-22		50 to 70	65 to 90	30 to 40	40 to 50	
FPQ3230-T-22		100 to 150	130 to 195	45 to 60	60 to 75	
FPQ3535-T-22		130 to 180	170 to 230	70 to 80	90 to 100	

Note: The output wattage is specified for conditions using TOKIN's BH2 material and the temperature rise of the transformer being $\Delta T < 45^\circ\text{C}$ within range of the operating flux density.



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List of Core Set Shapes

Ordering Code System

EB 40 - P 12 12 - F
 ① ② ③ ④ ⑤ ⑥

- ① Series
 EBBobbins for FEI and FEE Cores
 ERBBobbins for FEER Cores
 PQBBobbins for FPQ Cores
- ② Size of Core
- ③ Type of Pin
- ④ Type of Placing 11: Horizontal Type, 12: Vertical Type
- ⑤ Number of Pins
- ⑥ Material F: Phenor Resin

Description of Abbreviations

Ae : Section Area of Core (cm²)
 W : Weight of Core (g/Set)

The dimension without the specification of tolerance in-dicates the typical value.

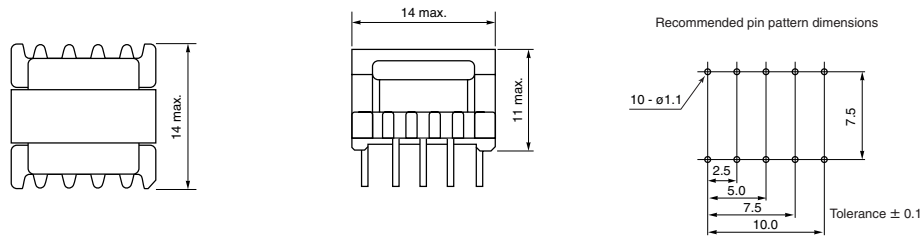
Outline drawing

[mm] as the unit for dimensions not specified otherwise.
 The top view is shown for the pin pattern dimensions not specified otherwise.



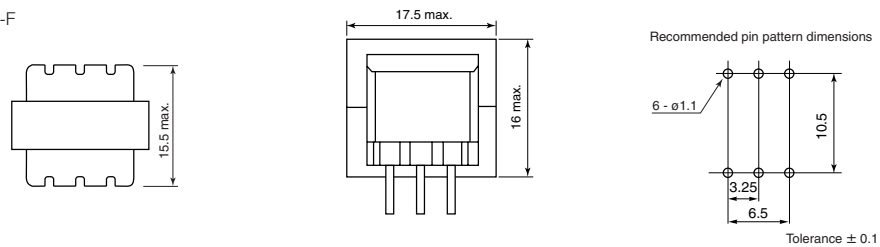
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article name	Core Ae	W	Bobbin
FEI12.5	0.15	1.9	EB12.5-P1210-F

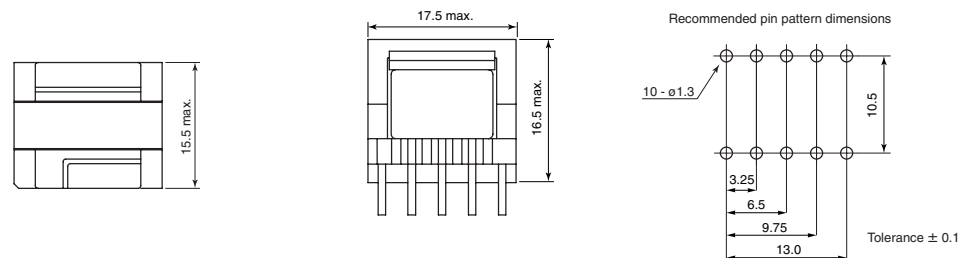


article name	Core Ae	W	Bobbin
FEI16	0.19	3.2	EB16-P1206-F, EB16-P1210-FA
FEE16	0.19	3.3	

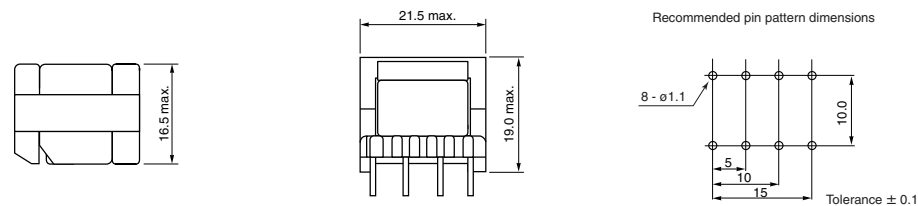
●EB16-P1206-F



●EB16-P1210-FA

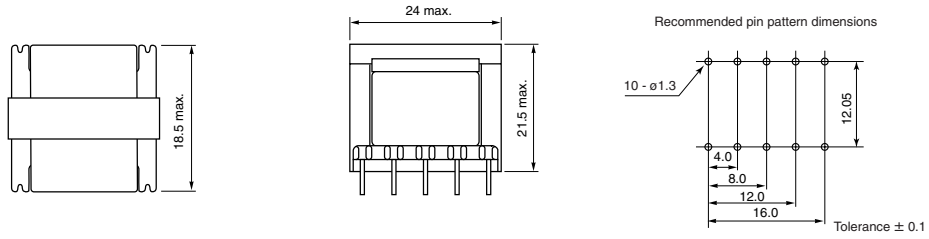


article name	Core Ae	W	Bobbin
FEI19	0.23	4.4	EB19-P1208-F
FEE19	0.23	4.8	

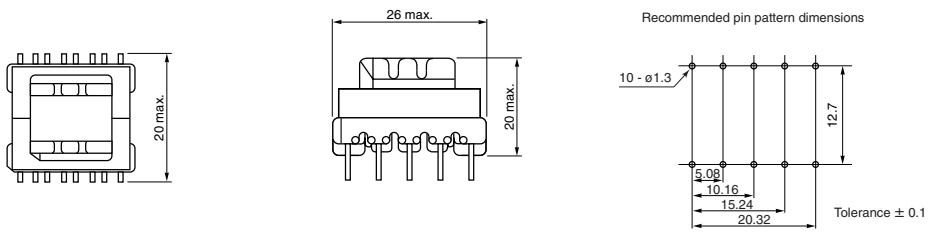


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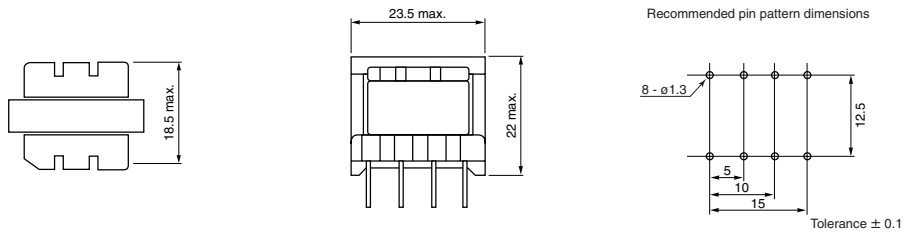
article name	Core		Bobbin
	Ae	W	
FEI22	0.41	8.8	EB22-P1210-F
FEE22	0.42	8.8	



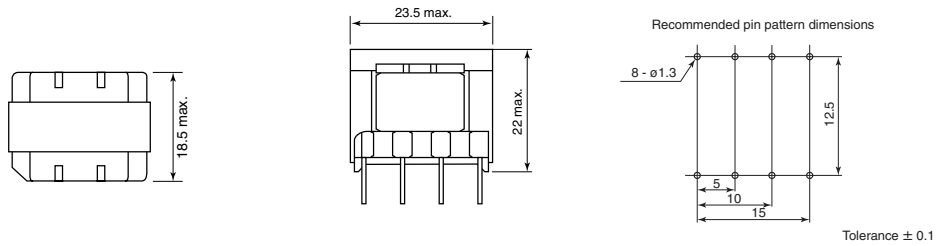
article name	Core		Bobbin
	Ae	W	
FEI22	0.41	8.8	EB22-P1110-FA
FEE22	0.42	8.8	



article name	Core		Bobbin
	Ae	W	
FEI22S	0.36	7.7	EB22S-P1208-F

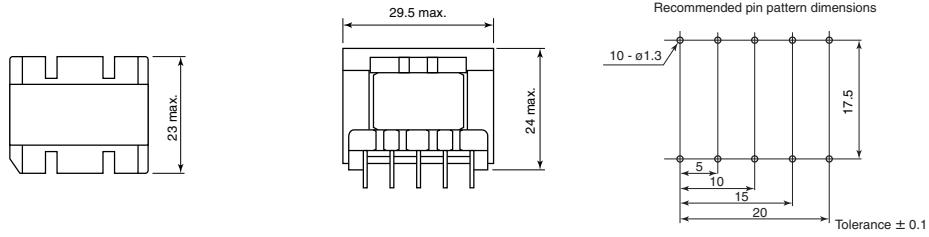


article name	Core		Bobbin
	Ae	W	
FEI25	0.41	11.0	EB25-P1208-F

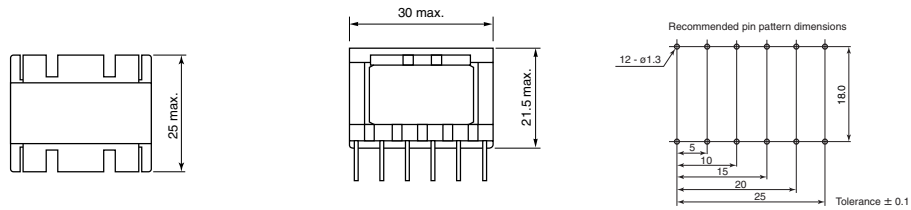


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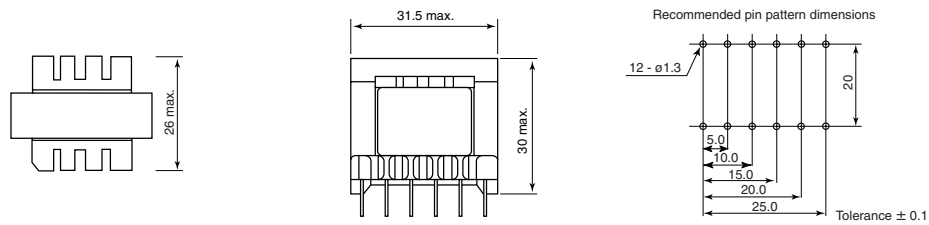
article name	Core Ae	W	Bobbin
FEI28	0.85	24.0	EB28-P1210-F
FEE28S	0.87	21.5	



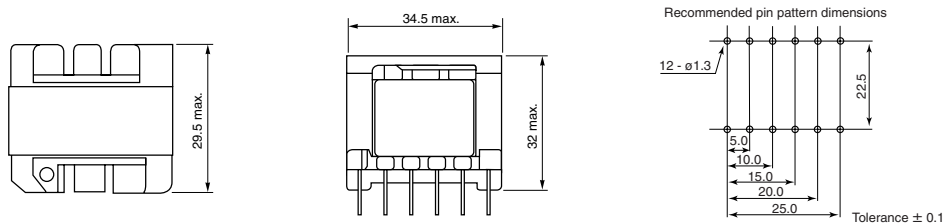
article name	Core Ae	W	Bobbin
FEI28	0.85	24.0	EB28-P1212-F
FEE28S	0.87	21.5	



article name	Core Ae	W	Bobbin
FEI30	1.11	35.0	EB30-P1212-F
FEE30	1.11	33.0	

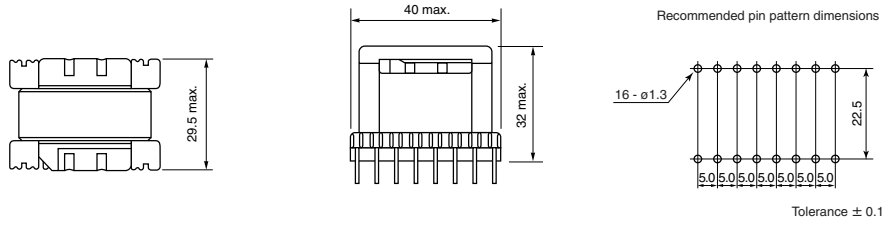


article name	Core Ae	W	Bobbin
FEI33	1.18	41.5	EB33-P1212-FS

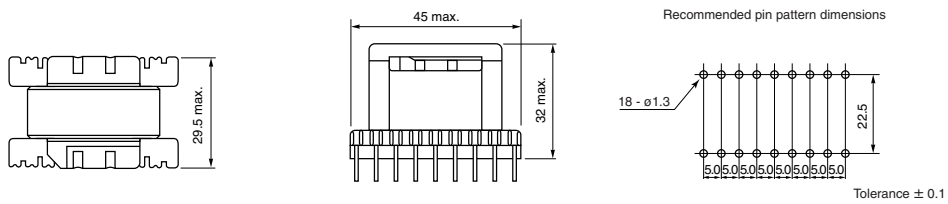


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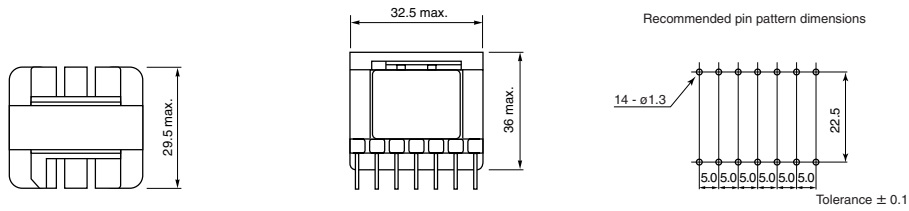
article name	Core		Bobbin
	Ae	W	
FEI33	1.18	41.5	EB33-P1216-F



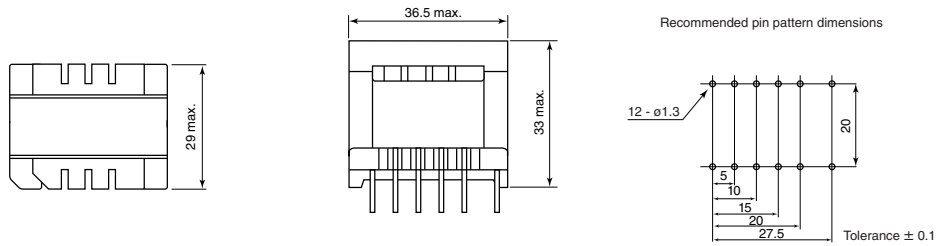
article name	Core		Bobbin
	Ae	W	
FEI33	1.18	41.5	EB33-P1218-F



article name	Core		Bobbin
	Ae	W	
FEI33	1.18	41.5	EB33-P1214-F1



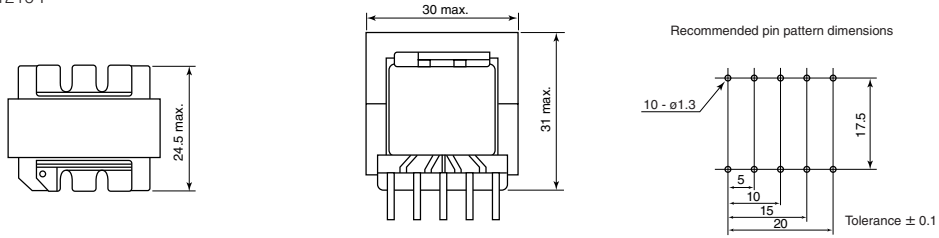
article name	Core		Bobbin
	Ae	W	
FEI35S	1.2	41.5	EB35S-P1212-F



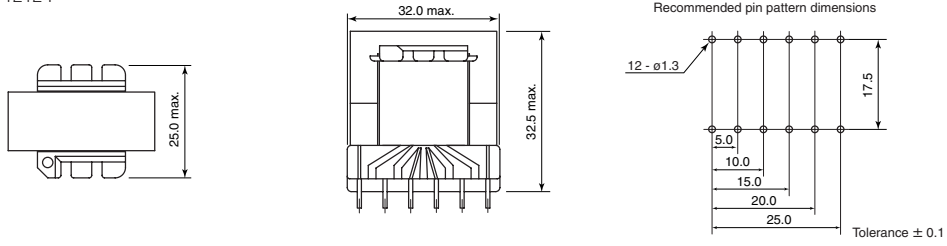
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article name	Core		Bobbin
	Ae	W	
FEER28	0.85	28.5	ERB28-P1210-F、ERB28-P1212-F

●ERB28-P1210-F

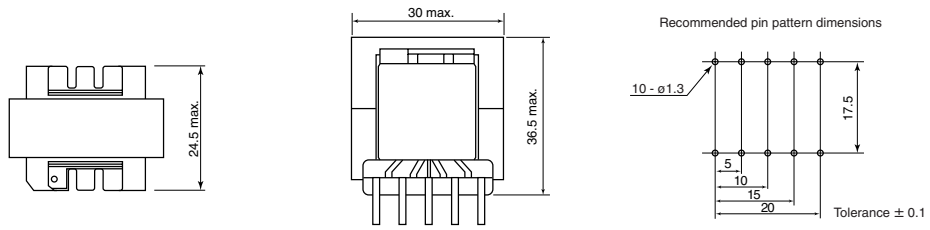


●ERB28-P1212-F

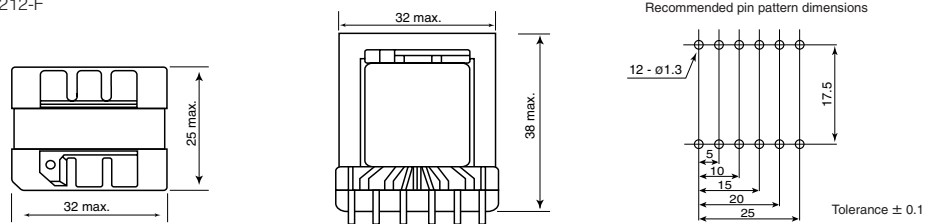


article name	Core		Bobbin
	Ae	W	
FEER28L	0.85	33.2	ERB28L-P1210-F、ERB28L-P1212-F

●ERB28L-P1210-F

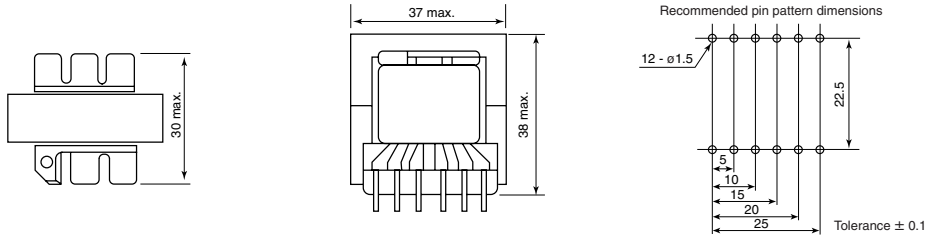


●ERB28L-P1212-F

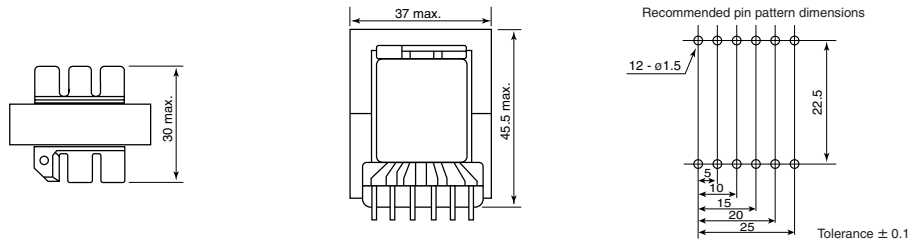


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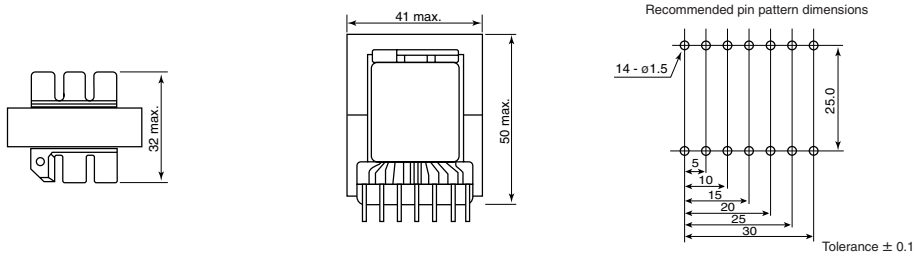
article name	Core Ae	W	Bobbin
FEER35	1.10	45.0	ERB35-P1212-F



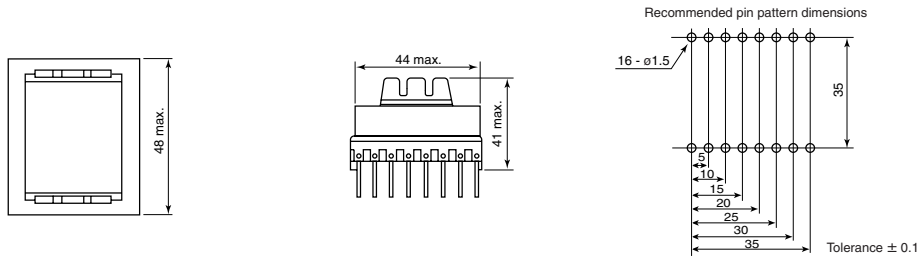
article name	Core Ae	W	Bobbin
FEER35L	1.08	50.7	ERB35L-P1212-F



article name	Core Ae	W	Bobbin
FEER39L	1.32	70.0	ERB39L-P1214-F

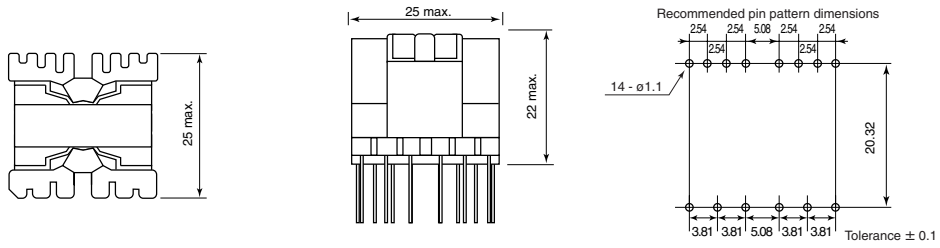


article name	Core Ae	W	Bobbin
FEER39L	1.32	70.0	ERB39L-P1116-F

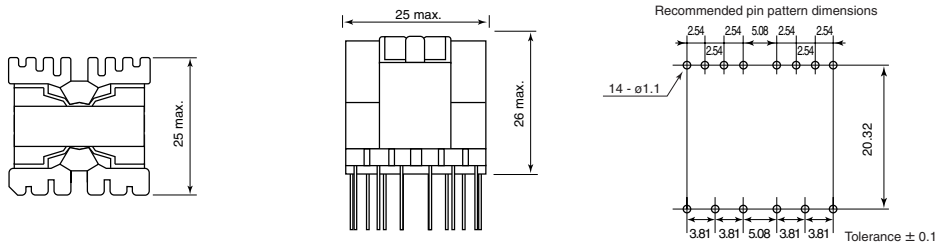


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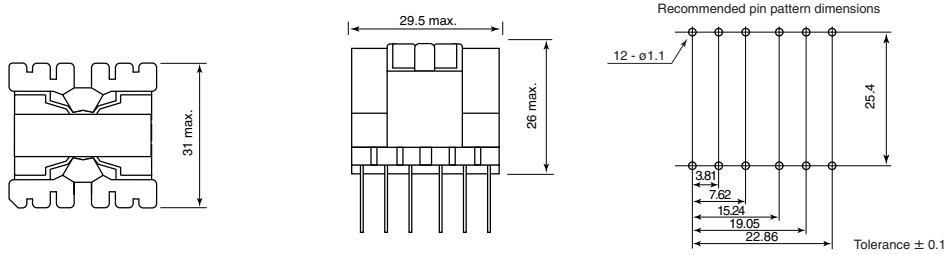
article name	Core		Bobbin
	Ae	W	
FPQ2016-T-22	0.62	13.0	PQB2016-P1214



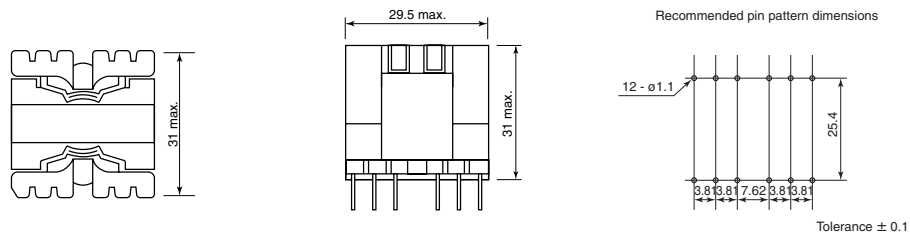
article name	Core		Bobbin
	Ae	W	
FPQ2020-T-22	0.62	5.0	PQB2020-P1214



article name	Core		Bobbin
	Ae	W	
FPQ2620-T-22	1.19	31.0	PQB2620-P1212

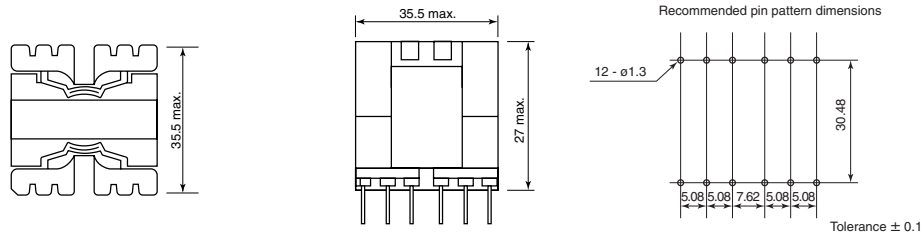


article name	Core		Bobbin
	Ae	W	
FEQ2625-7-22	1.19	36.0	PQB2625-P1212-F

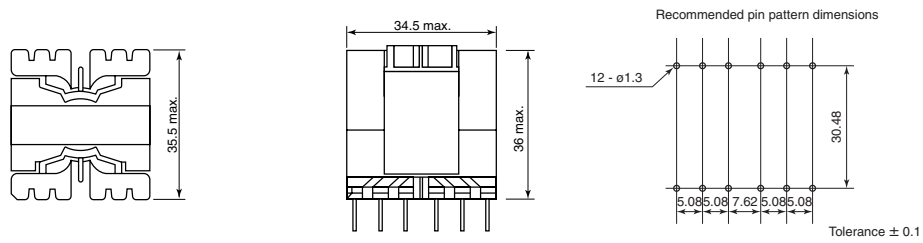


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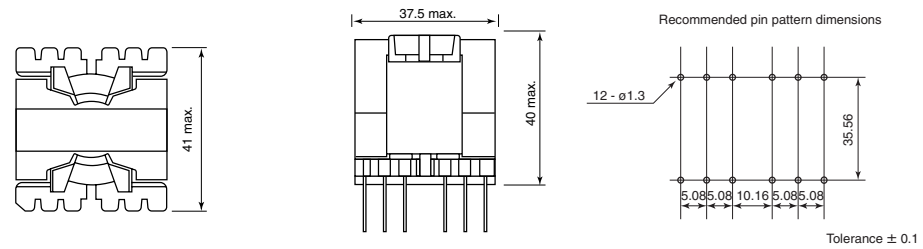
article name	Core		Bobbin
	Ae	W	
FPQ3220-T-22	1.70	42.0	PQB3220-P1212



article name	Core		Bobbin
	Ae	W	
PQB3220-T-22	1.61	55.0	PQB3230-P1212-F



article name	Core		Bobbin
	Ae	W	
FPQ3535-T-22	1.96	73.0	PQB3535-P1212-FA



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Notes for Handling

- Confirm the required operating conditions for each product before using it.
(Applying excess load may damage the transformer.)
- Avoid subjecting the terminals of the transformer to excessive stress.
(This can damage the wiring.)
- Avoid handling the product while holding the transformer part after it is mounted on the board.
(This can loosen the core or damage the wiring.)
- Never use any product that has been dropped .
(A cracked core can cause unsatisfactory characteristics .)



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Custom transformer series (Through-hole type)

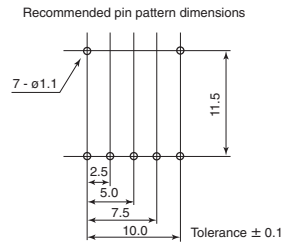
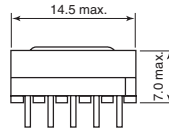
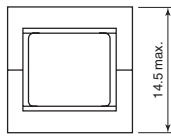
Output Wattage	Core Size	Bobbin
4W	FEY13.5 / 6.75 / 3.0	EYB13.5-P1107-F
4W	FEY12.7 / 12 / 4	EYB12-P1107-F7
5W	FEY16 / 14.5 / 5	EYB16-P1107-F1
6W	FEE12.6	EEB12.6-P1109-F
7W	FEY16D / 14.2 / 5.5	EYB16D-P1110-F
15W	FEI22S	EB22S-P1211-F
15W	FEI22S	EB22S-P1210-F、EB22S-C
18W	FEE22	EEHB22-P1110-F
20W	FEE23	EB23-P1209-FA
40W	FEEH28	ERB28S-P1216-FD
40W	FEEH28	EHB28-P1214-F2
50W	FEY28D	EYB28-P1112-F

Circuit condition: Flyback at= 100 kHz
 *Contact us individually regarding safety standard complied models.

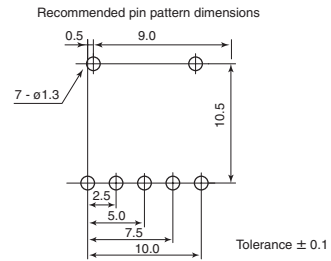
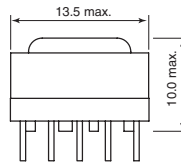
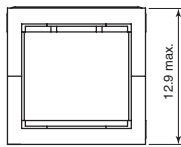


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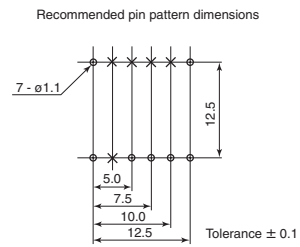
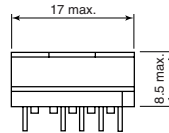
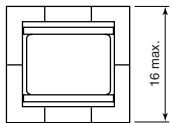
article name	Core		Bobbin
	Ae	W	
FEB13.5/6.75/3.0	0.097	1.7	EYB13.5-P1107-F



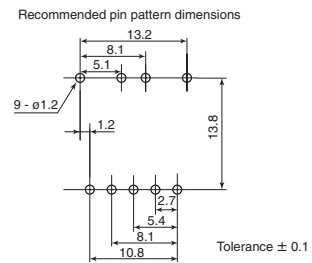
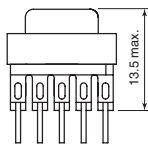
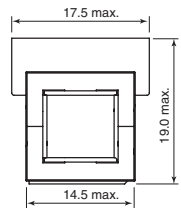
article name	Core		Bobbin
	Ae	W	
FEY12.7/12/4	0.107	1.6	EYB12-P1107-F7



article name	Core		Bobbin
	Ae	W	
FEY16/14.5/5	0.1593	3.0	EYB16-P1107-F1

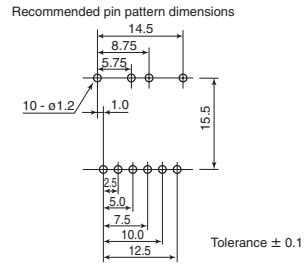
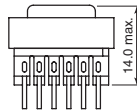
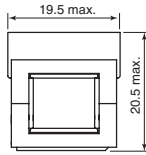


article name	Core		Bobbin
	Ae	W	
FEE12.6	0.124	2.0	EEB12.6-P1109-F

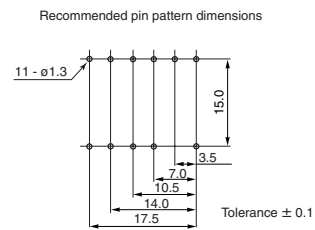
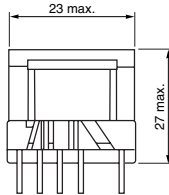
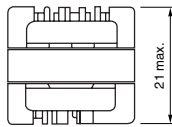


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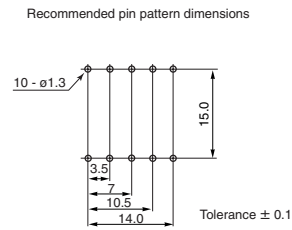
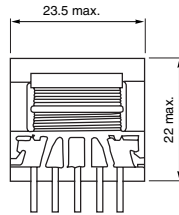
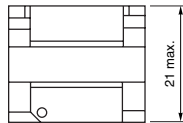
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FEY16D/14.2/5.5	0.236	4.1	EYB16D-P1110-F



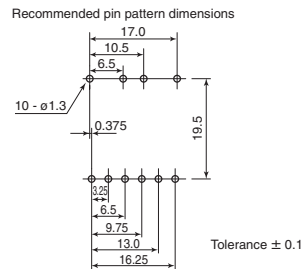
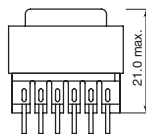
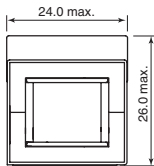
article name	Core Ae	W	Bobbin
FEI22S	0.36	7.7	EB22S-P1211-F



article name	Core Ae	W	Bobbin
FEI22S	0.36	7.7	EB22S-P1210-F, EB22S-C



article name	Core Ae	W	Bobbin
FEE22	0.502	11.7	EEHB22-P1110-F



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Precautions



- The names of the products and the specifications in this catalog are subject to change without notice for the sake of improvement. The manufacturer also reserves the right to discontinue any of these products. At the time of delivery, please ask for specifications sheets to check the contents in order to use the products properly and safely.
- Descriptions in this catalog regarding product characteristics and quality are based solely on discrete components. When using these components, be sure to check the specifications with the component in question mounted on the products.
- The manufacturer's warranty will not cover any disadvantage or damage caused by improper use of the products that deviates from the characteristics, specifications, or conditions for use described in this catalog.
- The products in this catalog are intended for use in ordinary electronic products. If any of these products are to be used in special applications requiring extremely high reliability, such as in aviation equipment and nuclear power controllers where product defects might pose a safety risk, please consult your NEC TOKIN sales representatives.
- Though the manufacturer has taken all possible precautions to ensure the quality and reliability of its products, improper use of products may result in bodily injury, fire, or similar accident. If you have any questions regarding the use of the products in question, please consult your NEC TOKIN sales representatives.
- Please be advised that the manufacturer accepts no responsibility for any infraction by users of the manufacturer's products on third party patents or industrial copyrights. The manufacturer is responsible only when such infractions are attributable to the structural design of the product and its manufacturing process.
- Export Control
For customers outside Japan
NEC TOKIN products should not be used or sold for use in the development, production, stockpiling or utilization of any conventional weapons or mass-destructive weapons (nuclear weapons, chemical or biological weapons, or missiles), or any other weapons.
For customers in Japan
For products which are controlled items subject to the "Foreign Exchange and Foreign Trade Law" of Japan, the export license specified by the law is required for export.
- This catalog is current as of March 2010.



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